

10

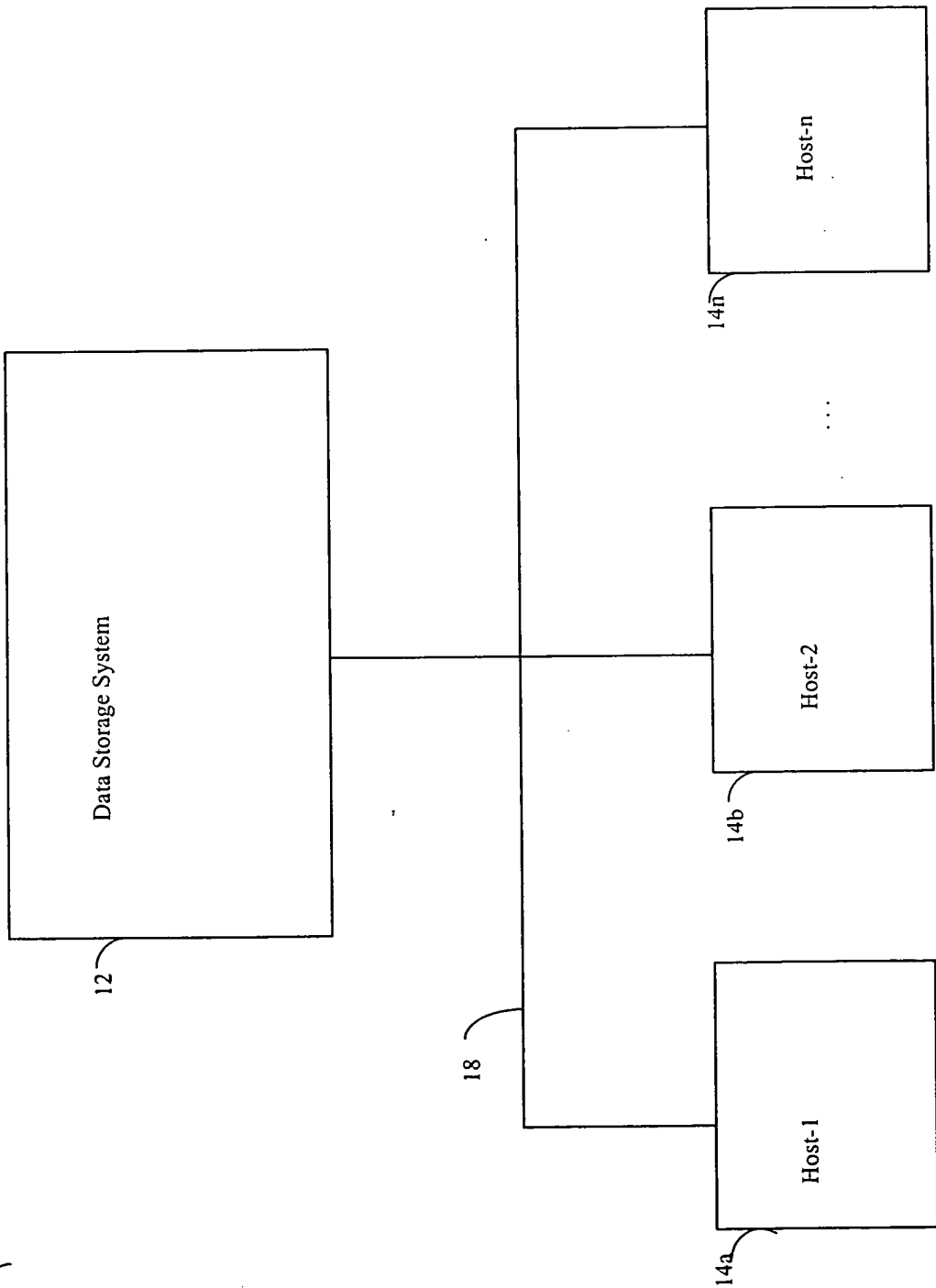


FIGURE 1

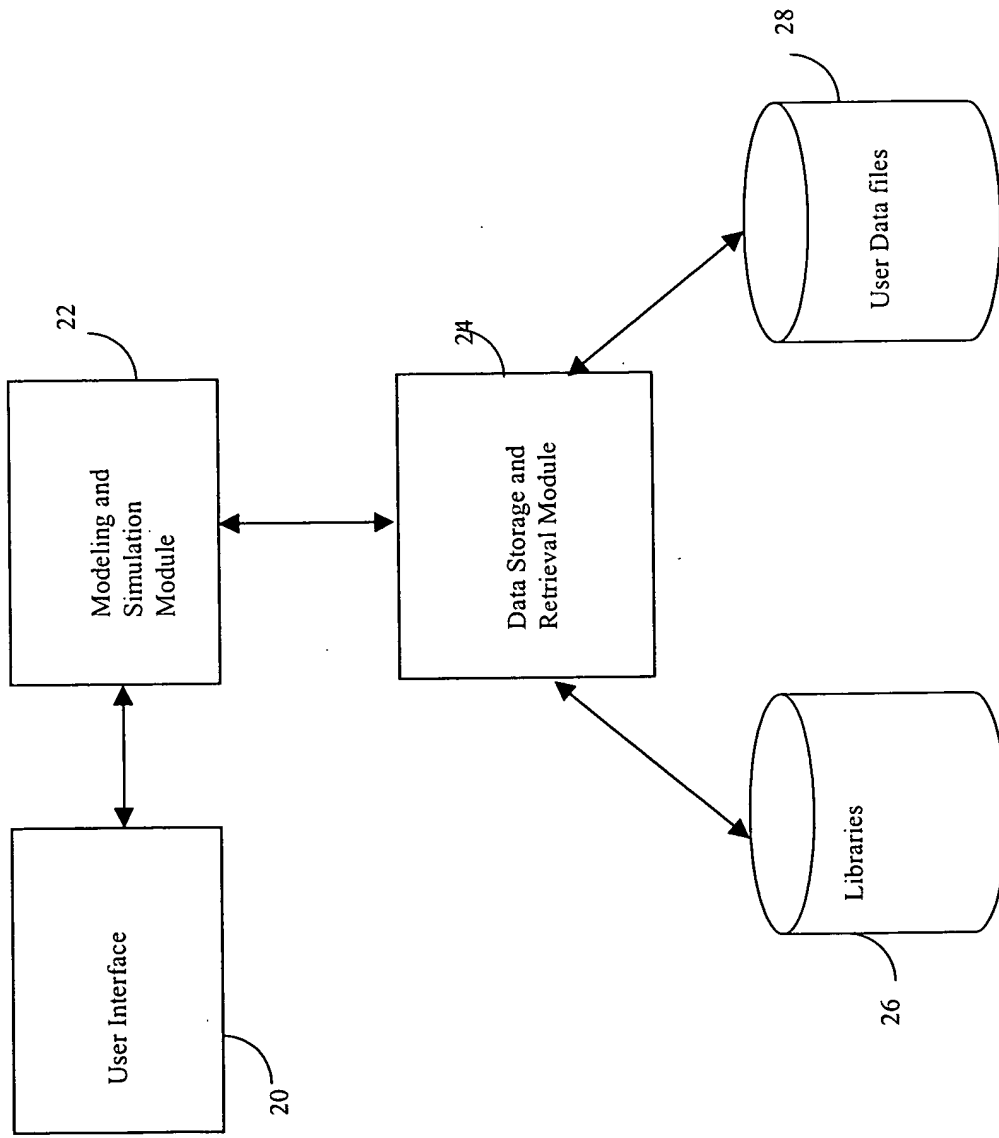


FIGURE 2

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FIGURE 3, 54

30

50 52

Model Navigator

New | Model Library | User Models | Multiphysics | Preferences

56

34

Dimension
C 1-D C 2-D

Independent variables: x y

32

AC Power Electromagnetics
Conductive Media DC
Diffusion
Electrostatics
Magnetostatics
Heat Transfer
Incompressible Navier-Stokes
Structural Mech., Plane Stre
Structural Mech., Plane Stra
PDE, coefficient form
PDE, general form

33a

>>
<<

33b

Solver type: Linear stationary

Solution form: Coefficient

40

42

Conductive Media DC
Heat Transfer

58

36

Application mode name: ht2

38

Dependent variables: T2

44

46

48

Application mode name: ht

Dependent variables: T

Sub mode: Standard

OK Cancel

31a 31b

FIGURE 4

PDE Specification/ht

Equation: $\rho \cdot C \cdot T' \cdot \nabla \cdot (k \nabla T) = Q + h \cdot (T_{\text{ext}} \cdot T) + C_{\text{trans}} \cdot (T_{\text{ambtrans}} \cdot T^4) \cdot T = \text{temperature}$

Subdomain selection

1

Name: 1

☒ Active in this subdomain

PDE coefficients ☒ Unlock

Coefficient	Value	Description
ρ	8930	Density
C	340	Heat capacity
k	384	Coeff. of heat conduction
Q	$1./(10 \cdot (1 + \alpha \cdot (T - T_0))) \cdot 1$	Heat source
h_{trans}	0	Convect. heat transf. coeff.
T_{ext}	0	External temperature
C_{trans}	0	User-defined constant
T_{ambtrans}	0	Ambient temperature

☒ On top

OK Cancel Apply

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FIGURE 3.5

70

Boundary Conditions/ht

Equation: $T = T_0$

Boundary selection

1
2
3
4
5
6
7

Name: 1

☒ Enable borders

Boundary coefficients ☒ Unlock

Quantity	Value	Description
<input type="radio"/> q	0	Heat flux
<input type="radio"/> h	0	Heat transfer coefficient
<input type="radio"/> T_{inf}	0	External temperature
<input type="radio"/> C	0	Problem-dependent constant
<input type="radio"/> T_{amb}	0	Ambient temperature
<input type="radio"/> $n \cdot (k \cdot \text{grad} T) = 0$		Insulation/symmetry
<input checked="" type="radio"/> T	300	Temperature
<input type="radio"/> $T = 0$		Zero temperature

☒ On top

OK Cancel Apply

72

74a

74

74b

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FIGURE 4/6

-continued-

80

Equation: $n(c \nabla u + \alpha u \gamma) + q \bar{u} = g$ $h^T \lambda$ $\lambda^T h u = 1$

82a 82b 82c 82d 84a 84b 84c 84d

q g h i

Boundary selection

1
2
3
4

Name:

q coefficient

u	v	T	
1	0	0	ps
0	1	0	ps
0	0	0	ht

94

On top

OK

Cancel

Apply

92a 92b 92c

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88

96

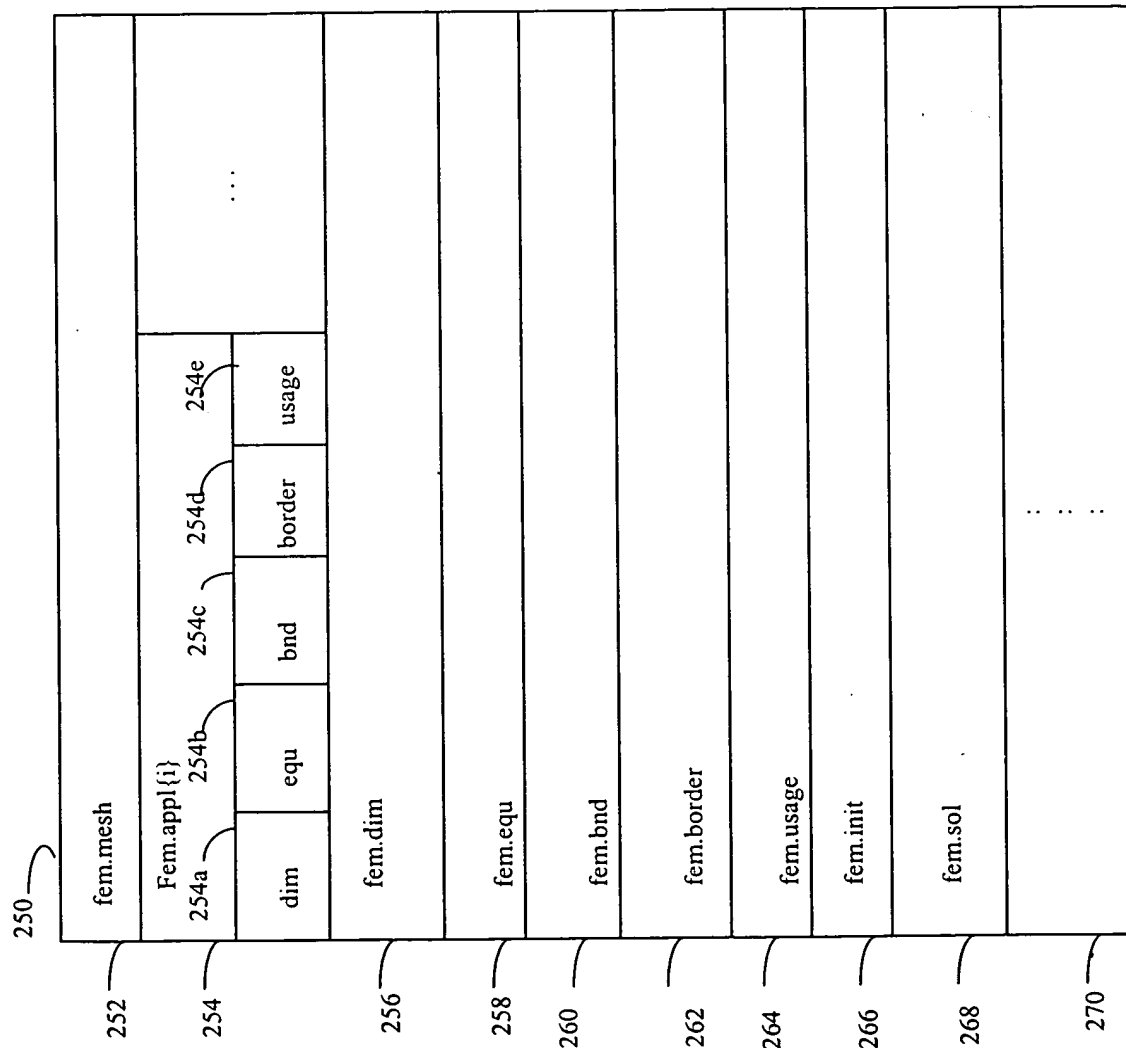


FIGURE 6A

FIGURE 5/7

Solver Parameters

General | Adaption | Nonlinear | Timestepping | Eigenvalue | Multigrid | Multiphysics

Solve for variables

Show variables

Structural Mechanics, Plane Stress (ps)
Heat Transfer (ht)

Update mechanism for initial value u

Update u

Update u automatically

Use interpolation

Use solution number. 1

Solve OK Cancel Apply

110

114a

124

112

116

116d

118a

118b

118c

118d

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FIGURE 8

$$\begin{cases}
 d_{a\ lk} \frac{\partial u_k}{\partial t} - \frac{\partial}{\partial x_j} \left(c_{lkji} \frac{\partial u_k}{\partial x_i} + \alpha_{lkj} u_k - \gamma_{lj} \right) + \beta_{lki} \frac{\partial u_k}{\partial x_i} + a_{lk} u_k = f_l & \Omega \\
 n_j \left(c_{lkji} \frac{\partial u_k}{\partial x_i} + \alpha_{lkj} u_k - \gamma_{lj} \right) + q_{lk} u_k = g_l - h_{ml} \lambda_m & \partial\Omega \\
 h_{ml} u_l = r_m & \partial\Omega
 \end{cases}
 \begin{matrix}
 142 \\
 146a \\
 146b
 \end{matrix}
 \left. \begin{matrix} \\ \\ \end{matrix} \right\} 146$$

FIGURE 9

$$\begin{cases}
 d_{a\ lk} \frac{\partial u_k}{\partial t} + \frac{\partial \Gamma_{lj}}{\partial x_j} = F_l & \Omega \\
 -n_j \Gamma_{lj} = G_l + \frac{\partial R_m}{\partial u_l} \lambda_m & \partial\Omega \\
 0 = R_m & \partial\Omega
 \end{cases}
 \begin{matrix}
 152 \\
 154a \\
 154b
 \end{matrix}
 \left. \begin{matrix} \\ \\ \end{matrix} \right\} 154$$

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Figure 10

$$\begin{array}{l}
 \left. \begin{array}{l}
 \gamma_{ij} = \Gamma_{ij} \\
 c_{ikj} = - \frac{\partial \Gamma_{ij}}{\partial \left(\frac{\partial u_k}{\partial x_i} \right)} \\
 \beta_{iki} = - \frac{\partial F_i}{\partial \left(\frac{\partial u_k}{\partial x_i} \right)} \\
 g_i = G_i \\
 q_{ik} = - \frac{\partial G_i}{\partial u_k}
 \end{array} \right\} \begin{array}{l}
 f_i = F_i \\
 \alpha_{ikj} = - \frac{\partial \Gamma_{ij}}{\partial u_k} \\
 a_{ik} = - \frac{\partial F_i}{\partial u_k} \\
 r_i = R_i \\
 h_{ik} = - \frac{\partial R_i}{\partial u_k}
 \end{array}
 \end{array}$$

FIGURE 11.

$$\begin{cases}
 \Gamma_{lj} = -c_{lkji} \frac{\partial u_k}{\partial x_i} - \alpha_{lkj} u_k + \gamma_{lj} \\
 F_l = f_l - \beta_{lki} \frac{\partial u_k}{\partial x_i} - a_{lk} u_k \\
 G_l = g_l - q_{lk} u_k \\
 R_m = r_m - h_{ml} u_l
 \end{cases}$$

FIG 12

$$\begin{aligned}
 & \int_{\Omega} \left(\left(c_{lkji} \frac{\partial u_k}{\partial x_i} + \alpha_{lkj} u_k \right) \frac{\partial v}{\partial x_j} + \left(d_{alk} \frac{\partial u_k}{\partial t} + \beta_{lki} \frac{\partial u_k}{\partial x_i} + a_{lk} u_k \right) v \right) dx + \\
 & \int_{\partial\Omega} q_{lk} u_k v ds = \int_{\Omega} \left(\gamma_{lj} \frac{\partial v}{\partial x_j} + f_l v \right) dx + \int_{\partial\Omega} (g_l - h_{ml} \lambda_m) v ds \\
 & \int_{\partial\Omega} \mu h_{mk} u_k ds = \int_{\partial\Omega} \mu r_m ds
 \end{aligned}$$

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FIG 13

$$302 \left\{ \begin{array}{l} \int_{\Omega} \left(\Gamma_{lj} \frac{\partial v}{\partial x_j} + F_l v - d_{alk} \frac{\partial u^k}{\partial t} v \right) dx + \int_{\partial\Omega} \left(G_l + \frac{\partial R_m}{\partial u_l} \lambda_m \right) v ds = 0 \\ \int_{\partial\Omega} R_m \mu ds = 0 \end{array} \right.$$

FIG 14

$$304 \left\{ U_k(x) = \sum_{I=1}^{N_p} U_{I,k} \phi_I(x), \right.$$

$$\Lambda_m(x) = \sum_{K=1}^{N_e} \sum_{L=1}^n \Lambda_{K,L,m} \psi_{K,L}(x),$$

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FIG 15

$$\begin{aligned}
 & \int_{\tau} \left(c_{lkji} U_{I,k} \frac{\partial \phi_I}{\partial x_i} + \alpha_{lkj} U_{I,k} \phi_I \right) \frac{\partial \phi_J}{\partial x_j} dx + \\
 & \int_{\tau} \left(d_{a l k} \frac{\partial U_{I,k}}{\partial t} \phi_I + \beta_{lki} U_{I,k} \frac{\partial \phi_I}{\partial x_i} + a_{lk} U_{I,k} \phi_I \right) \phi_J dx + \\
 & \int_{\partial \tau} q_{lk} U_{I,k} \phi_I \phi_J ds = \int_{\tau} \left(\gamma_{IJ} \frac{\partial \phi_J}{\partial x_j} + f_I \phi_J \right) dx + \\
 & \int_{\partial \tau} (g_I - h_{mI} \Lambda_{K,L,m} \psi_{K,L}) \phi_J ds
 \end{aligned}$$

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FIG 16

$$2) \int \frac{\partial}{\partial \tau} h_{mk} U_{I,k} \phi_I \Psi_{K,L} ds = \int \frac{\partial}{\partial \tau} r_m \Psi_{K,L} ds$$

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FIG 17

$$3^2 \left\{ \int_{\tau} \left(\Gamma_{lj} \frac{\partial \phi_j}{\partial x_j} + F_l \phi_j - d_{alk} \frac{\partial u_k}{\partial l} \phi_j \right) dx + \int_{\partial \tau} \left(G_l + \frac{\partial R_m}{\partial u_l} \Lambda_{K,L,m} \psi_{K,L} \right) \phi_j ds = 0 \right. \\ \left. \int_{\partial \tau} R_m \psi_{K,L} ds = 0 \right.$$

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FIG 18

$$\begin{aligned}
 310 \quad \overline{DA}_{(J,I),(I,k)} &= \int_{\tau} d_{a\,lk} \phi_I \phi_J dx \\
 C_{(J,I),(I,k)} &= \int_{\tau} c_{lkji} \frac{\partial \phi_I}{\partial x_i} \frac{\partial \phi_J}{\partial x_j} dx \\
 AL_{(J,I),(I,k)} &= \int_{\tau} \alpha_{lkj} \phi_I \frac{\partial \phi_J}{\partial x_j} dx \\
 BE_{(J,I),(I,k)} &= \int_{\tau} \beta_{lki} \frac{\partial \phi_I}{\partial x_i} \phi_J dx \\
 A_{(J,I),(I,k)} &= \int_{\tau} a_{lk} \phi_I \phi_J dx \\
 Q_{(J,I),(I,k)} &= \int_{\partial\tau} q_{lk} \phi_I \phi_J ds \\
 GA_{(J,I)} &= \int_{\tau} \gamma_{lj} \frac{\partial \phi_J}{\partial x_j} dx \\
 F_{(J,I)} &= \int_{\tau} f_I \phi_J dx \\
 G_{(J,I)} &= \int_{\partial\tau} g_I \phi_J ds \\
 H_{(K,L,m),(I,k)} &= \int_{\partial\tau} h_{mk} \phi_I \Psi_{K,L} ds \\
 R_{(K,L,m)} &= \int_{\partial\tau} r_m \Psi_{K,L} ds
 \end{aligned}$$

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FIG 19

$$320 \left\{ \begin{array}{l} DA \frac{\partial U}{\partial t} + (C + AL + BE + A + Q)U + H^T \Lambda = GA + F + G \\ HU = R \end{array} \right.$$

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sum

FIG 20

$$\left. \begin{array}{l} DA \frac{\partial U}{\partial t} + H^T \Lambda = GA + F + G \\ R = 0 \end{array} \right\}$$

FIG 21

$$326 \left\{ \begin{array}{l} J(U^{(k)}) \Delta U^{(k)} = -\rho(U^{(k)}) \\ U^{(k+1)} = U^{(k)} + \lambda_k \Delta U^{(k)} \end{array} \right.$$

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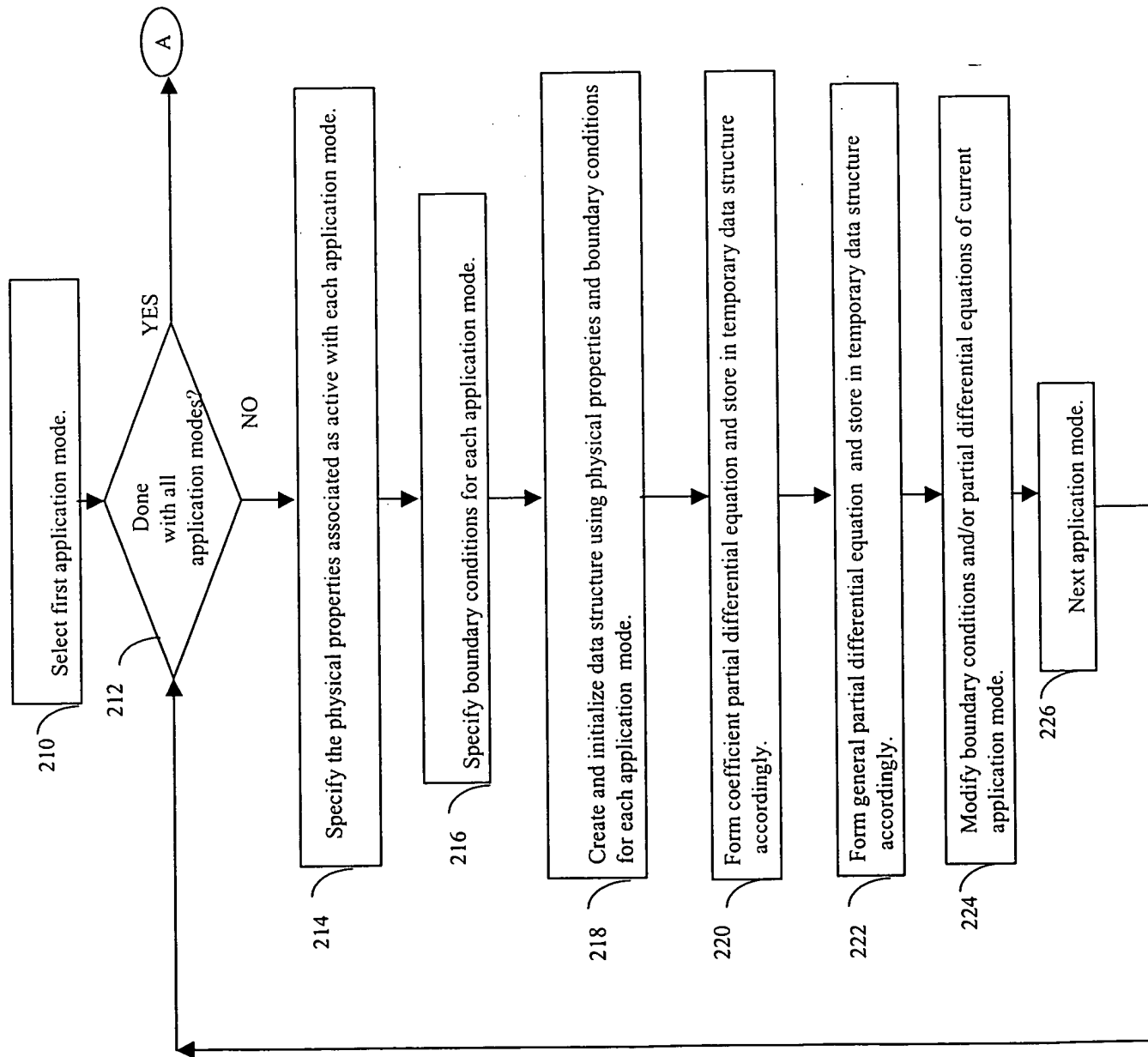


FIGURE 22

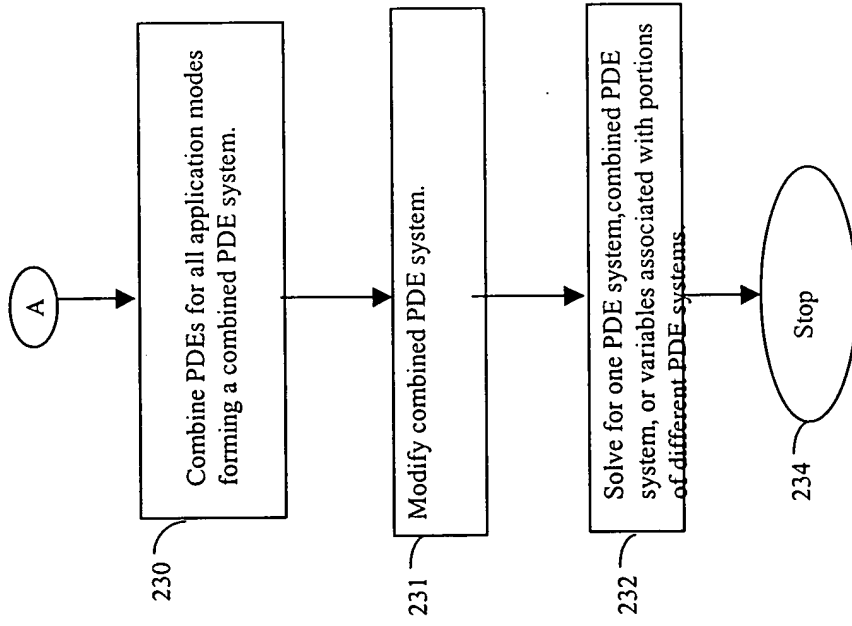
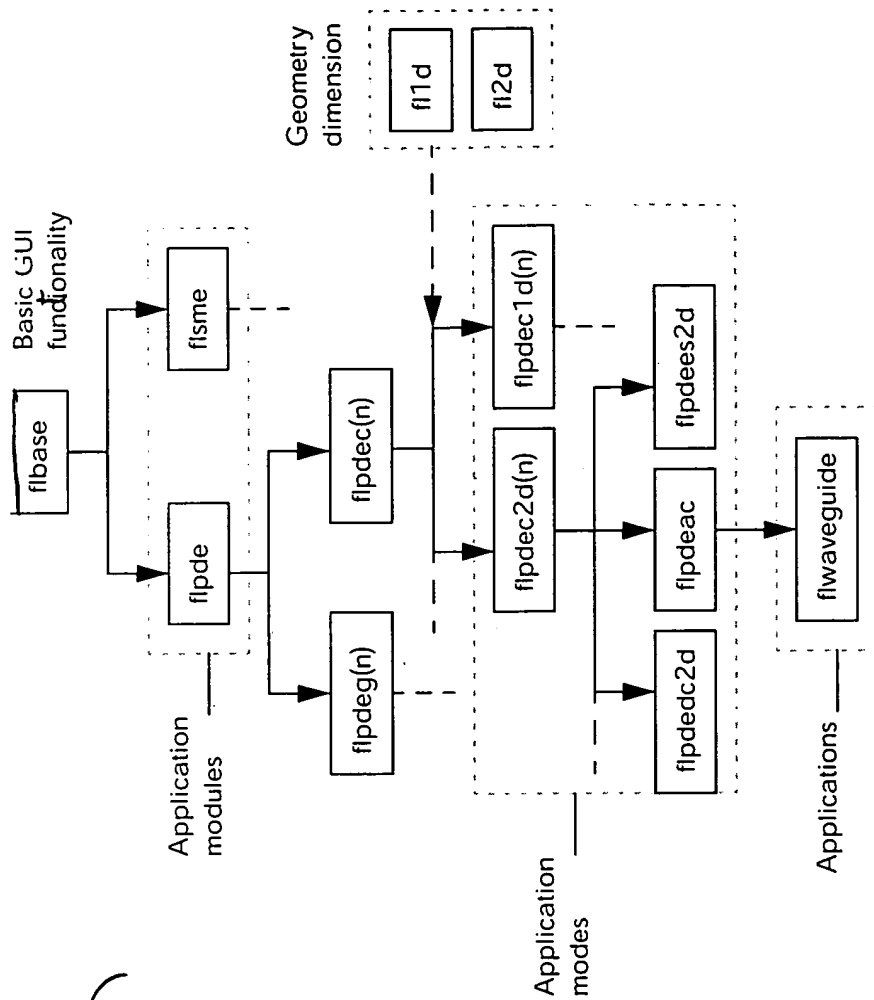


FIGURE 23



The class hierarchy of FEMLAB

Figure 24

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1-D Physics Application Modes		
Application mode	Class name	Parent class
Diffusion	flpdedf1d	flpdedf
Heat Transfer	flpdeht1d	flpdeht

S02

: 1-D PDE Application Modes		
Application mode	Class name	Parent class
Coefficient PDE model, n variables	flpdec1d(n)	flpdec(n)
General PDE model, n variables	flpdeg1d(n)	flpdeg(n)

S04

FIGURE 25

2-D Physics Application Modes

Application mode	Class name	Parent class
AC Power Electromagnetics	flpdeac	flpdec2d
Conductive Media DC	flpdedc2d	flpdedc
Diffusion	flpdedf2d	flpdedf
Electrostatics	flpdees2d	flpdees
Magnetostatics	flpdems2d	flpdems
Heat Transfer	flpdent2d	flpdent
Incompressible Navier-Stokes	flpdens2d	flpdens
Structural Mechanics, Plane Stress	flpdeps	flpdec2d
Structural Mechanics, Plane Strain	flpdepn	flpdec2d

Sub

Figure 26

PDE Application Modes

Application mode	Class name	Parent class
Coefficient PDE model, n variables	flpdec2d(n)	flpdec(n)
General PDE model, n variables	flpdeg2d(n)	flpdeg(n)

Sub

Application Object Properties

Property name	Description	Data type
dim	Names of the dependent variables	Cell array of strings
form	PDE form	String (coefficient/general)
name	Application name	String
parent	Parent class names	String, cell array of strings, or the empty matrix
sdim	Names of the independent variables (space dimensions)	Cell array of strings
submode	Name of current submode	String (std/wave)
tdiff	Time differentiation flag	String (on/off)

FIGURE 27

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```

function obj = myapp()
%MYAPP Constructor for a FEMLAB application object.
S12 obj.name = 'My first FEMLAB application';
    obj.parent = 'flpdeht2d';

% MYAPP is a subclass of FLPDEHT2D:
    p1 = flpdeht2d;
    obj = class(obj, 'myapp', p1);
    set(obj, 'dim', default_dim(obj));

```

FIGURE 28

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Physics Modeling Methods

Function	Purpose
appspec	Return application specifications.
bnd_compute	Convert application-dependent boundary conditions to generic boundary coefficients.
default_bnd	Default boundary conditions.
default_dim	Default names of dependent variables.
default_equ	Default PDE coefficients/Material parameters.
default_init	Default initial conditions.
default_sdim	Default space dimension variables.
default_var	Default application scalar variables.
dim_compute	Return dependent variables for an application.
equ_compute	Convert application-dependent material parameters to generic PDE coefficients.
form_compute	Return PDE form.
init_compute	Convert application-dependent initial conditions to generic initial conditions.
posttable	Define assigned variable names and post-processing information.

FIGURE 29

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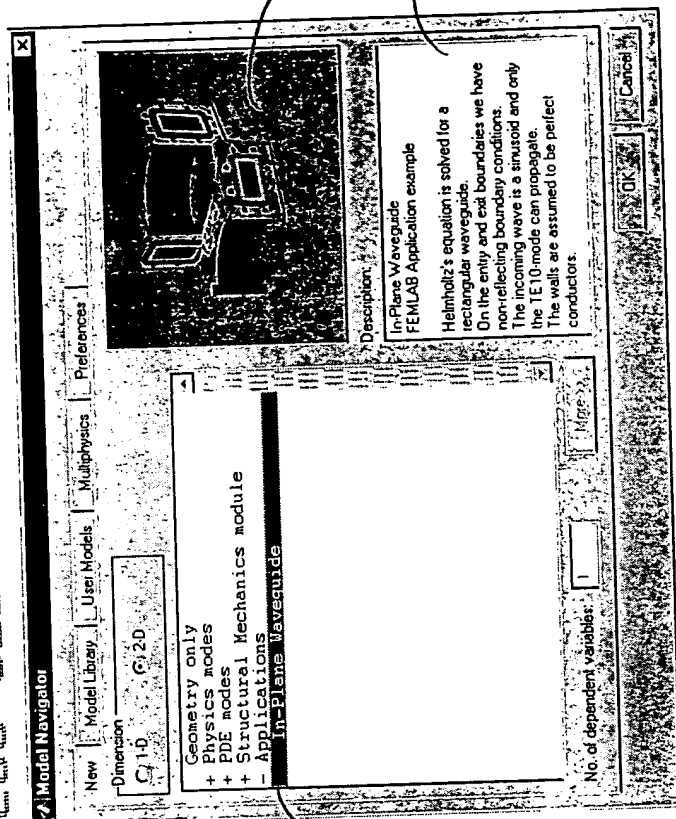


FIGURE 30

$$532 \quad \boxed{\Delta E_z + (2\pi i k)^2 E_z = 0}$$

$$532 \quad \boxed{k = \frac{1}{\lambda} = \frac{f}{c}}$$

$$534 \quad \boxed{\vec{n} \cdot (\nabla E_z) + 2\pi i k_x E_z = 4\pi i k_x \sin\left(\frac{\pi}{d}(y - y_0)\right)}$$

$$536 \quad \boxed{k^2 = k_x^2 + k_y^2}$$

$$538 \quad \boxed{k_x = \sqrt{\frac{1}{\lambda^2} - \frac{1}{(2d)^2}}$$

$$540 \quad \boxed{\vec{n} \cdot (\nabla E_z) + 2\pi i k_x E_z = 0}$$

$$542 \quad \boxed{E_z = 0}$$

$$544 \quad \boxed{f_c = \frac{c}{2d}}$$

FIGURE 31

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```
function obj = flwaveguide(varargin)
%FLWAVEGUIDE Constructor for a Waveguide application object.

obj.name = 'In-Plane Waveguide';
obj.parent = 'flpdeac';

% FLWAVEGUIDE is a subclass of FLPDEAC:
p1 = flpdeac;
obj = class(obj,'flwaveguide',p1);
set(obj,'dim',default_dim(obj));
```

FIGURE 32

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fem.user fields	
Field	Description
geomparam	1-by-2 structure of geometry parameters.
entrybnd	Index to the entry boundary.
exitbnd	Index to the exit boundary.
freqs	Frequency vector

FIGURE 33

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FILE NO. 34

FIGURE 35